

# Electrically Pumped SPASER

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# OUTLINE

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- **Data-Processing Devices**
- **SPPs and SPP losses**
- **SPP Amplification**
- **SPASER**
- **Active Plasmonic Interconnects**
- **Summary**

# Data-Processing Devices

## Nvidia GeForce GTX 680

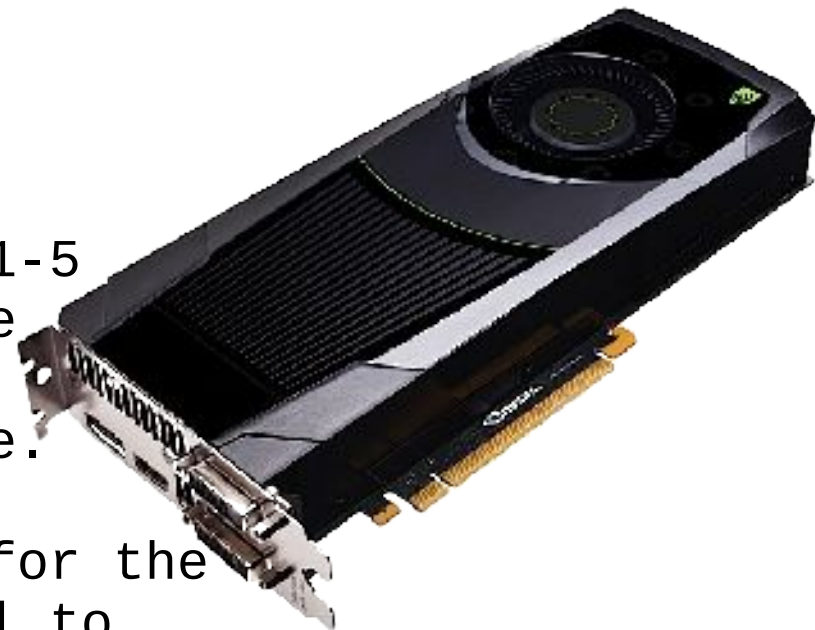
Number of CUDA cores: **1536**

Performance: **3.09 TFLOPS**

The problem is that after each 1-5 float point operations, one have to write or read information or transmit data to another core.

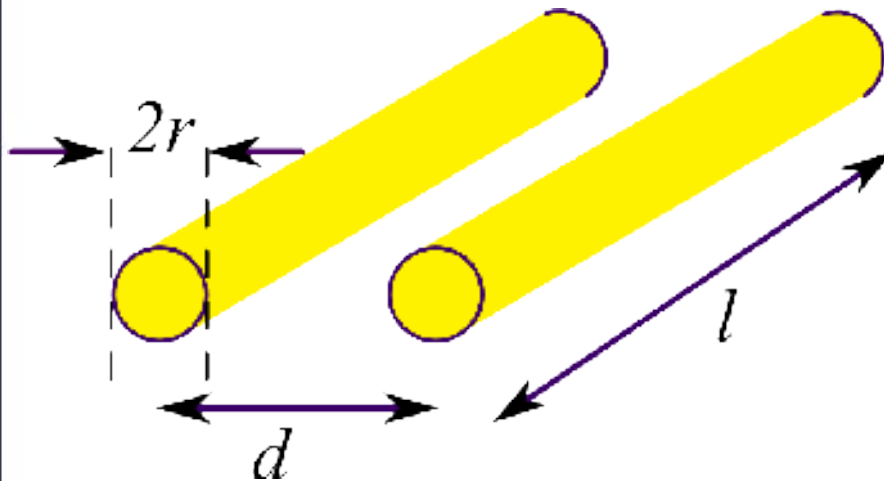
Ideally, the required bandwidth for the memory interface should be equal to **3090 GB/s** keeping a ratio of 1 byte/FLOP.

Actual bandwidth is only **192.2 GB/s**, but memory interface width is **256-bit**. So, we have **only 0.75 GB/s per line**.



# Data-Processing Devices: Copper Interconnects

## Twin-Wire Line Model



## Electrical interconnect limitations:

- 1) Propagation losses.
- 2)  $\tau=RC$  results in a delay and a rise time.
- 3) Miniaturizing the system doesn't reduce  $RC$  delay.

$$B < B_0 \frac{d^2}{l^2}, \text{ where } B_0 < 10^{16} \text{ bit/s}$$

$$\text{If } d < \frac{l}{1000}, \text{ then } \mathbf{B < 1 GB/s}$$

- D. Miller, H. Ozaktas, *Limit to the Bit-Rate Capacity of Electrical Interconnects from the Aspect Ratio of the System Architecture*, J. Parallel Distrib. Comput. **41**, 42–52 (1997).
- D. Miller, *Optical interconnects to electronic chips*, Appl. Opt. **49**, F59 (2010).

# Data-Processing Devices: Copper Interconnects

We have almost achieved the bandwidth limit of a single copper line (wire).

We can further increase the total bandwidth **only** by increasing the number of lines (wires)

**But it is not possible,** since today we have more than 256 lines, in chip-to-chip interconnects and much higher number in on-chip interconnects.

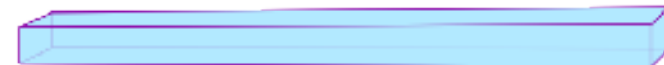
- D. Miller, H. Ozaktas, *Limit to the Bit-Rate Capacity of Electrical Interconnects from the Aspect Ratio of the System Architecture*, J. Parallel Distrib. Comput. 41, 42–52 (1997).
- D. Miller, *Optical interconnects to electronic chips*, Appl. Opt., 49, F59 (2010).

# Data-Processing Devices: *Optical Interconnects*

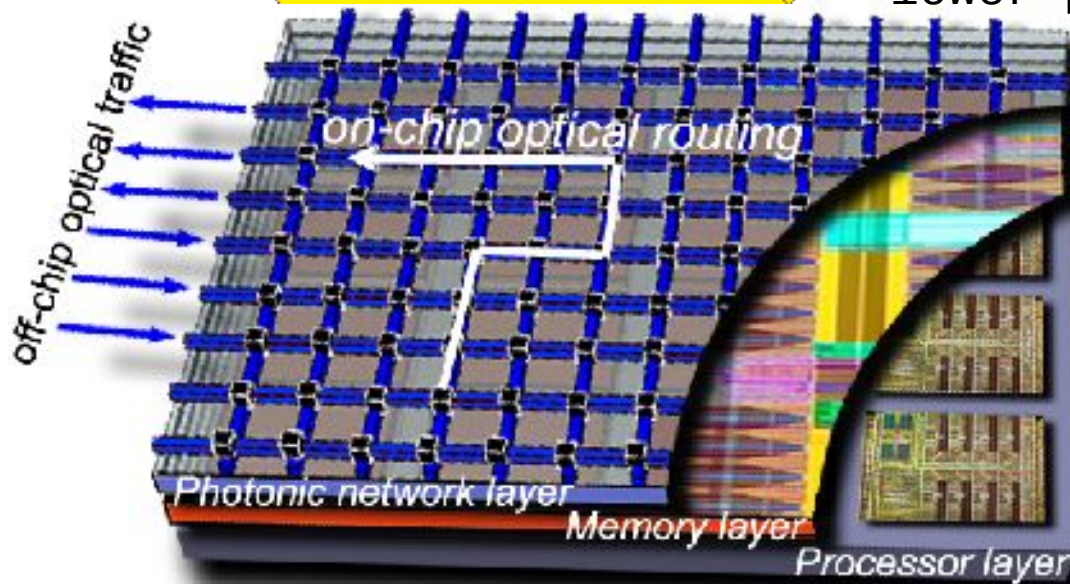
$N$  copper interconnects



1 optical interconnect



Higher bandwidth, lower delays,  
lower power consumption, similar  
interconnect dimensions,  
lower cross-talk



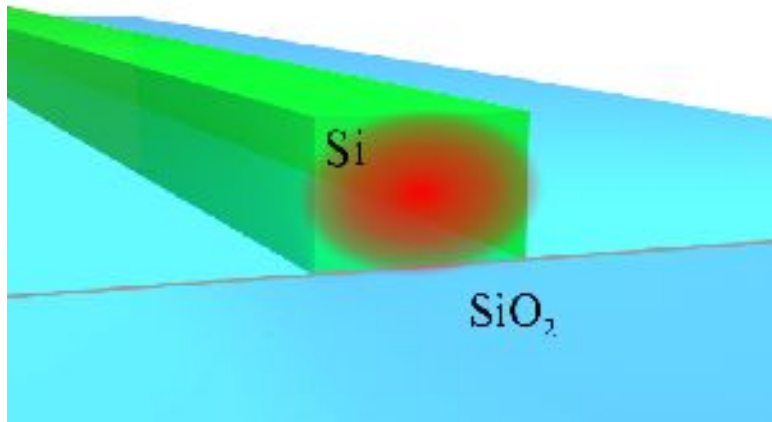
Utilizing on-chip  
optical interconnects,  
it becomes possible to  
achieve exaflop  
computing on a single  
chip.

Figure: <http://domino.research.ibm.com/>



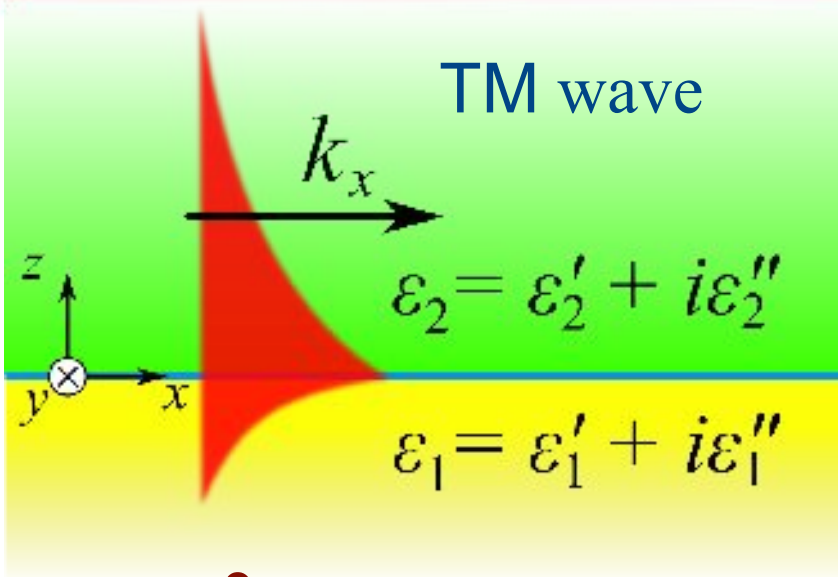
# Data-Processing Devices: Silicon Nanophotonics

CMOS integrated silicon nanophotonics gives silicon nanophotonics devices a possibility to share the same silicon layer with silicon transistors and design On-Chip and Chip-to-Chip interconnects.



Is it possible to suggest another approach, which is **more compact**, have the same bandwidth and the same delays?

# SPPs



Drude model:

$$\epsilon_1(\omega) = \epsilon_r - \frac{\omega_p^2}{\omega^2 + i\Gamma\omega}$$

$$\epsilon_1 = \text{Re}(\epsilon_1) + i \text{Im}(\epsilon_1)$$

$$\text{Re}(\epsilon_1) < 0$$

$$k_x = \text{Re}(k_x) + i \text{Im}(k_x)$$

$$\kappa_i = \sqrt{k_x^2 - \left(\frac{\omega}{c}\right)^2 \epsilon_i} \quad \text{- penetration constants}$$

$$\lambda_{\text{SPP}} = \frac{2\pi}{\text{Re}(k_x)} \quad \text{- SPP wavelength}$$

$$L_{\text{SPP}} = \frac{1}{2 \text{Im}(k_x)} \quad \text{- propagation length}$$

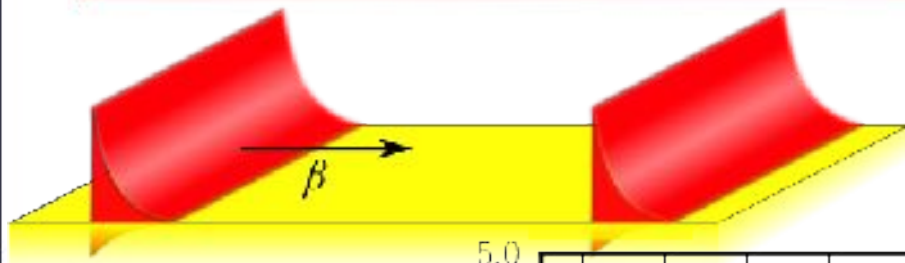
$$\rho_i = \frac{1}{\text{Re}(\kappa_i)} \quad \text{- penetration depths}$$

**SPP dispersion**

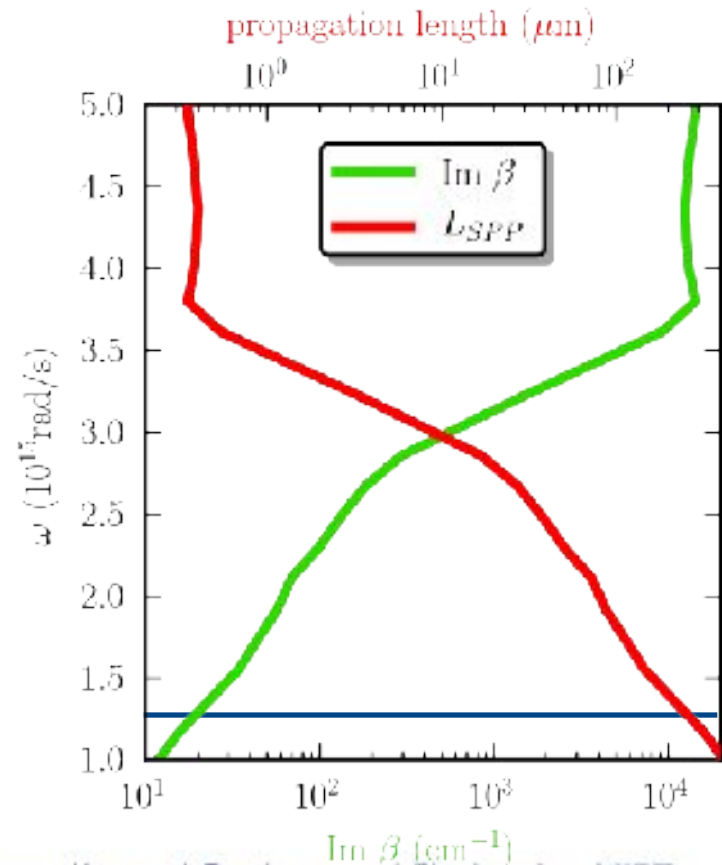
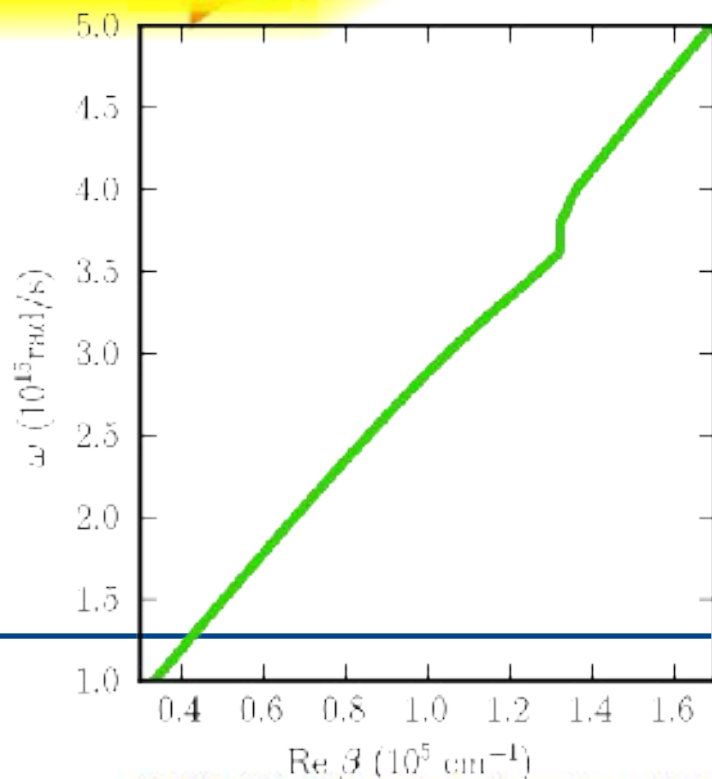
$$\kappa_1 \epsilon_2 = -\kappa_2 \epsilon_1$$



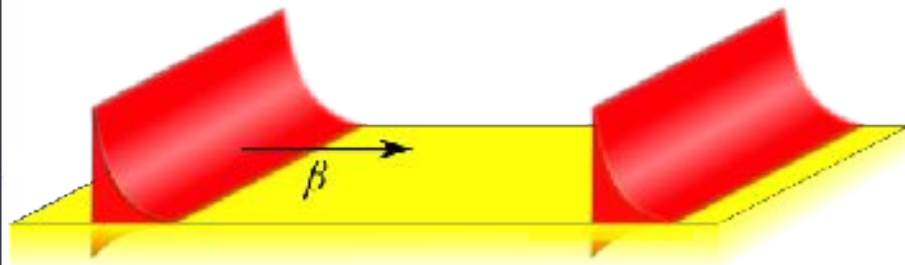
# SPP losses



1550 nm



# SPP losses



$$\lambda = 1.55 \text{ } \mu\text{m}$$

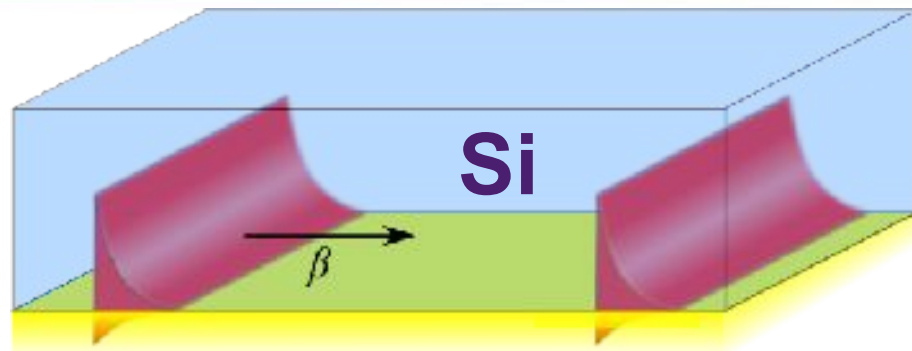
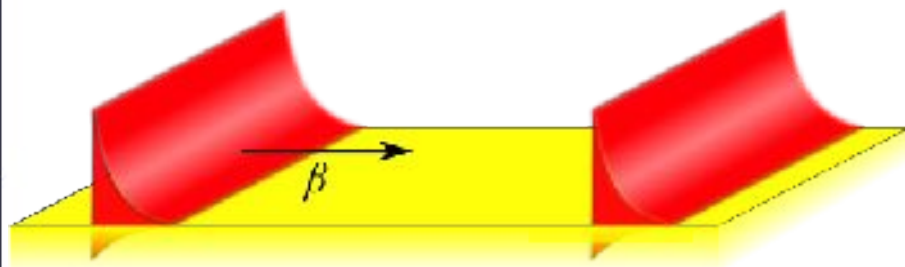
$$\lambda_{\text{SPP}} \approx 1.5 \text{ } \mu\text{m}$$

$$L_{\text{SPP}} \approx 270 \text{ } \mu\text{m}$$

$$\rho_{\text{Air}} \approx 2.5 \text{ } \mu\text{m}$$

$$\rho_{\text{Au}} \approx 0.023 \text{ } \mu\text{m}$$

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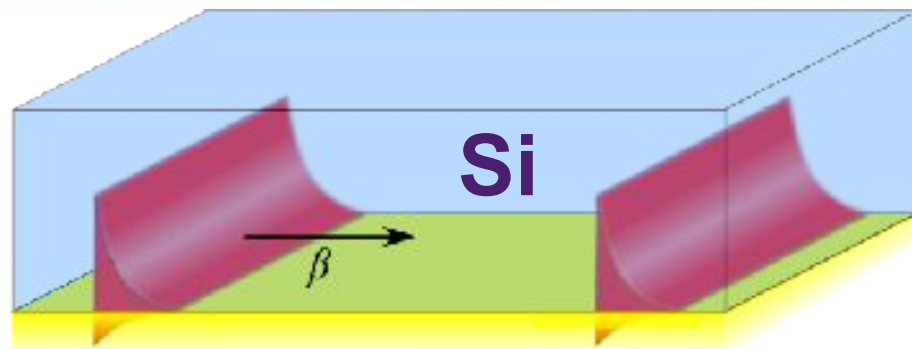
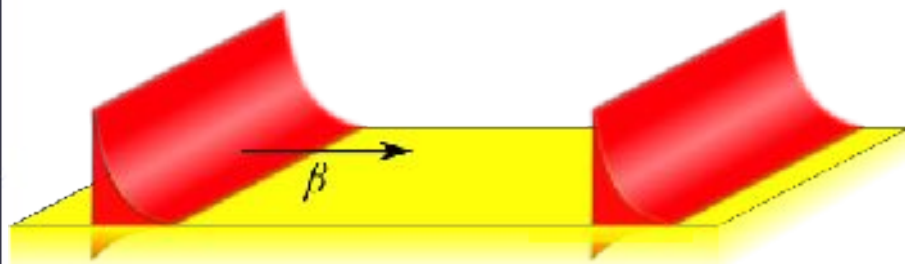
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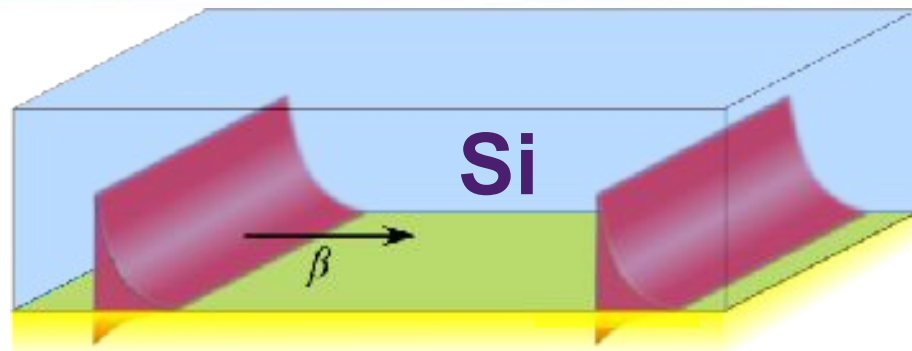
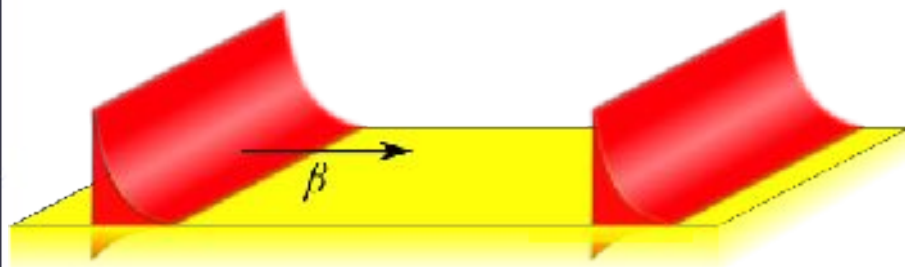
$$\lambda_{\text{SPP}} \approx 0.42 \text{ } \mu\text{m}$$

$$L_{\text{SPP}} \approx 5.8 \text{ } \mu\text{m}$$

$$\rho_{\text{Si}} \approx 0.2 \text{ } \mu\text{m}$$

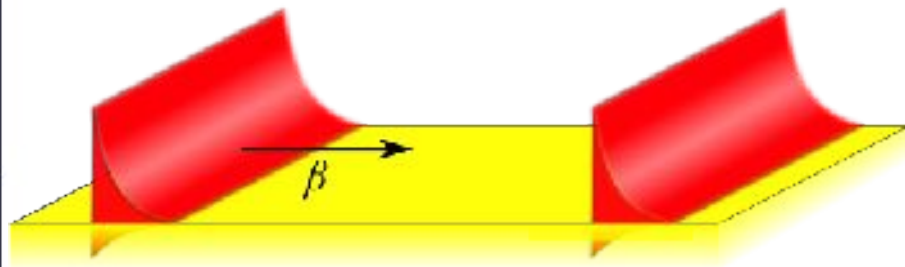
$$\rho_{\text{Au}} \approx 0.022 \text{ } \mu\text{m}$$

# SPP losses



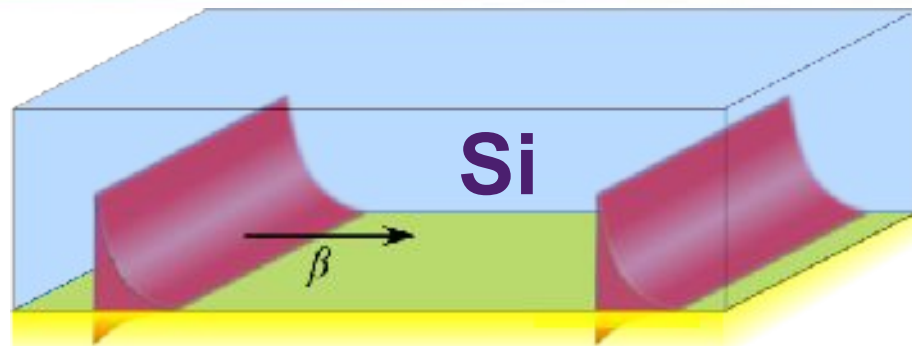
$$\text{Im } \beta \approx \frac{\omega}{2c} \frac{\epsilon_2^{3/2}}{\left(1 + \frac{\epsilon_2}{\text{Re } \epsilon_1}\right)^{3/2}} \frac{\text{Im } \epsilon_1}{(\text{Re } \epsilon_1)^2} \Rightarrow L_{\text{SPP}} \propto \frac{\left(1 + \frac{\epsilon_2}{\text{Re } \epsilon_1}\right)^{3/2}}{\epsilon_2^{3/2}}$$

# SPP losses



**Low-loss**  
**Not-confined**

$$\begin{aligned}\lambda &= 1.55 \mu\text{m} \\ \lambda_{\text{SPP}} &\approx 1.5 \mu\text{m} \\ L_{\text{SPP}} &\approx 270 \mu\text{m} \\ \rho_{\text{Air}} &\approx 2.5 \mu\text{m} \\ \rho_{\text{Au}} &\approx 0.023 \mu\text{m}\end{aligned}$$



**Very lossy**  
**Highly confined**

$$\begin{aligned}\lambda &= 1.55 \mu\text{m} \\ \lambda_{\text{SPP}} &\approx 0.42 \mu\text{m} \\ L_{\text{SPP}} &\approx 5.8 \mu\text{m} \\ \rho_{\text{Si}} &\approx 0.2 \mu\text{m} \\ \rho_{\text{Au}} &\approx 0.022 \mu\text{m}\end{aligned}$$

# SPP Amplification

High propagation losses due to Joule heating restrict the application of SPPs. Thus, one only way to overcome propagation losses is to partially or fully compensate Joule heating losses in the metal. This can be done by using an active gain medium placed near a metal surface and pumping it.

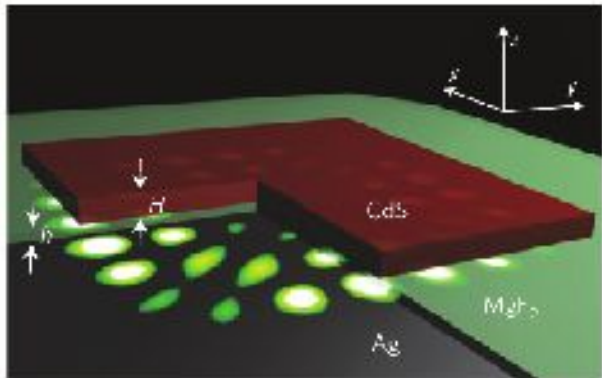
**PUMPING**



- A.M. Lakhani et al., *Plasmonic crystal defect nanolaser*, Opt. Express 19, 18237 (2011).
- R.A. Flynn et al., *A room-temperature semiconductor spaser operating near 1.5  $\mu\text{m}$* , Opt. Express 19, 8954 (2011).
- R.-M. Ma et al., *Room-temperature sub-diffraction-limited plasmon laser by total internal reflection*, Nat. Mat. 10, 110 (2011).
- J.K. Kitur et al., *Stimulated Emission of Surface Plasmon Polaritons in a Microcylinder Cavity*, Phys. Rev. Lett. 106, 183903 (2011).
- and many other papers

# SPP Amplification: Optical Pumping

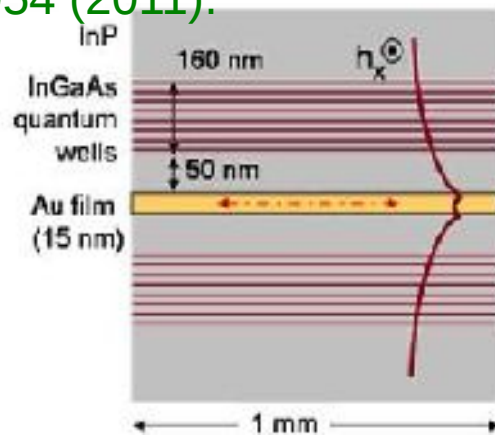
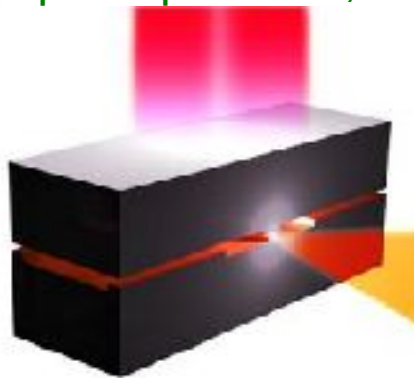
-R.-M. Ma, R.F. Oulton, V.J. Sorger, G. Bartal & X. Zhang, *Room-temperature sub-diffraction-limited plasmon laser by total internal reflection*, Nat. Mat. 10, 110 (2011).



**Pumping:** frequency-doubled, mode-locked Ti:Sa laser ( $\lambda=405$  nm, pulse length 100 fs).

**Threshold:** of the order of **1 GW/cm<sup>2</sup>** at **room temperature** and about **60 MW/cm<sup>2</sup>** at **10 K**.

-R. A. Flynn et al., *A room-temperature semiconductor spaser operating near 1.5  $\mu\text{m}$* , Opt. Express 19, 8954 (2011).



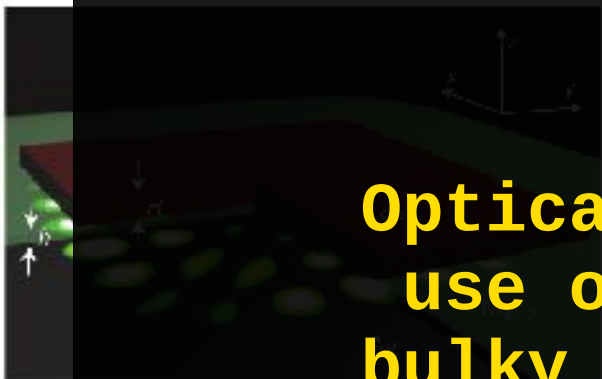
**Pumping:** pulsed laser ( $\lambda=1.06$   $\mu\text{m}$ , pulse length 140 ns)

**Threshold:** about **60 kW/cm<sup>2</sup>** at **room temperature**



# SPP Amplification: Optical Pumping

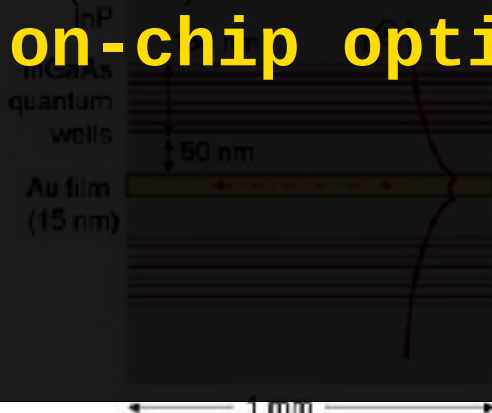
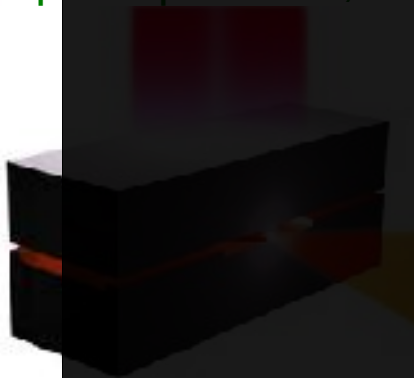
-R. M. Ma, R.F. Oulton, V.J. Sorger, G. Bartal & X. Zhang, Room-temperature sub-diffraction-limited plasmon laser by total internal reflection, Nat. Mat. 10, 110 (2011).



Pumping: frequency-doubled, mode-locked Ti:Sa laser ( $\lambda=405$  nm, pulse length 100 fs).

Optical pumping requires the use of external high-power bulky pump lasers and is not feasible in ultracompact on-chip optical circuits

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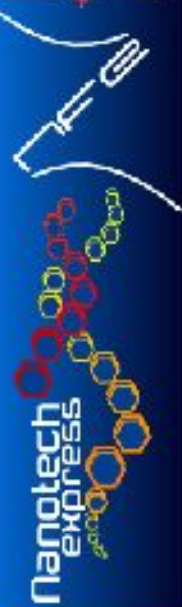
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# SPP Amplification

Is it possible to design a COMPACT plasmonic structure with NEGLIGIBLY SMALL PROPAGATION LOSSES?

Requirements:

- Compact pumping
- Full loss compensation
- Compatibility with compact plasmonic and optical waveguides



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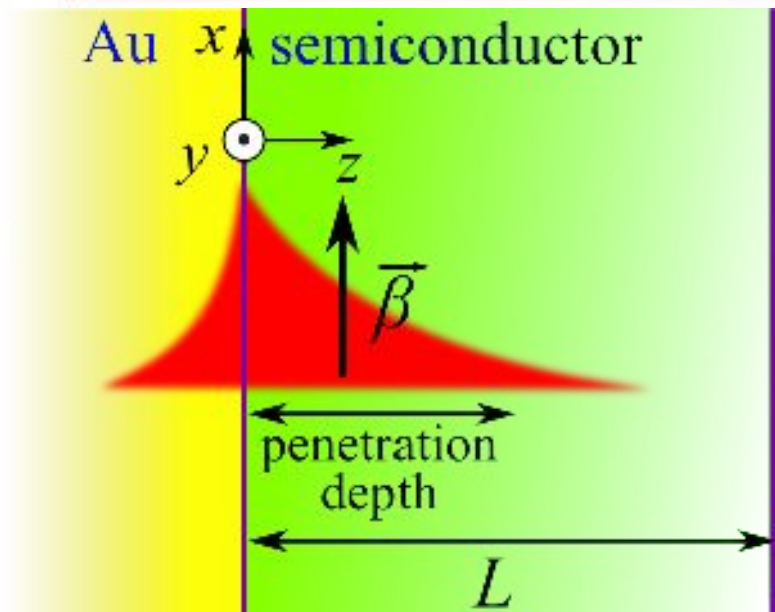
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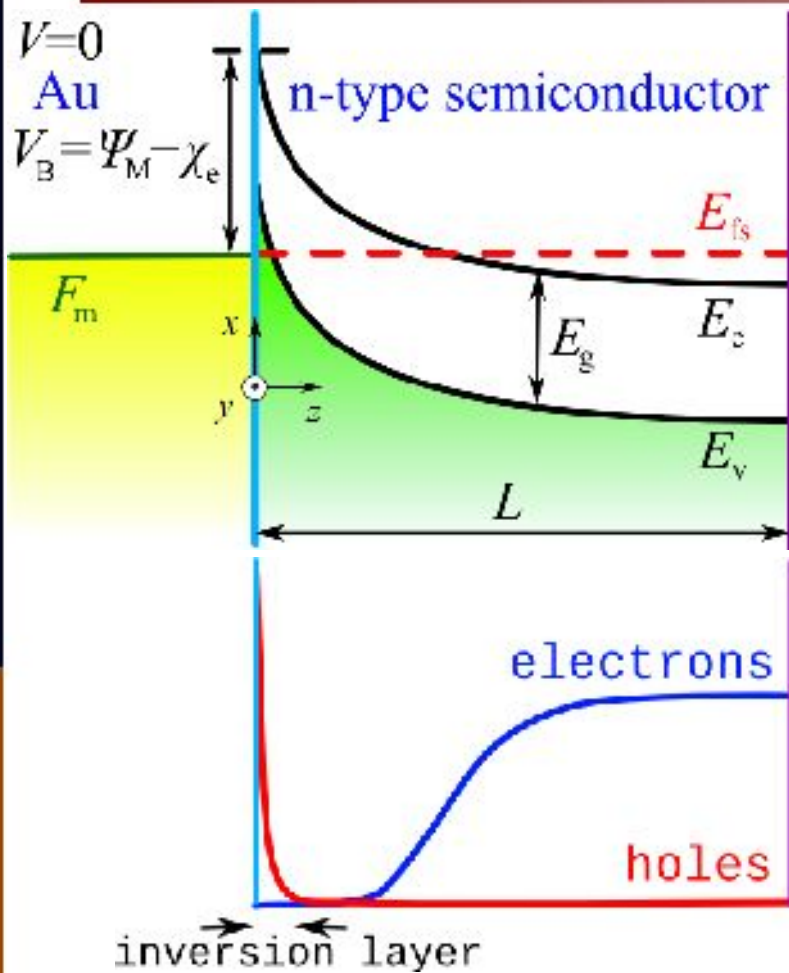
**The answer is electric pumping!**

- D.Yu. Fedyanin, *Toward an electrically pumped spaser*, Opt. Lett. **37**, 404 (2012).
- D.Yu. Fedyanin, A.V. Arsenin, *Surface plasmon polariton amplification in metal-semiconductor structures*, Opt. Express **19**, 12524-12531 (2011).
- D.Yu. Fedyanin, A.V. Arsenin, *Au/InAs Surface Plasmon Polariton Amplifier and SPASER // AIP Conf. Proc. 1398*, 70-72 (2011).
- D.Yu. Fedyanin, A.V. Arsenin, *Semiconductor Surface Plasmon Amplifier Based on a Schottky Barrier Diode // AIP Conf. Proc. 1291*, 112-114 (2010).

# SPP Amplification



# SPP Amplification: Electric Pumping



Usually, Schottky diodes are treated as majority carrier devices. However, the situation changes drastically when the barrier height exceeds the half of the bandgap. In this case an inversion layer is formed near the metal-semiconductor contact. Under sufficient forward bias this carriers are injected into the bulk of the semiconductor and recombine with majority carriers.

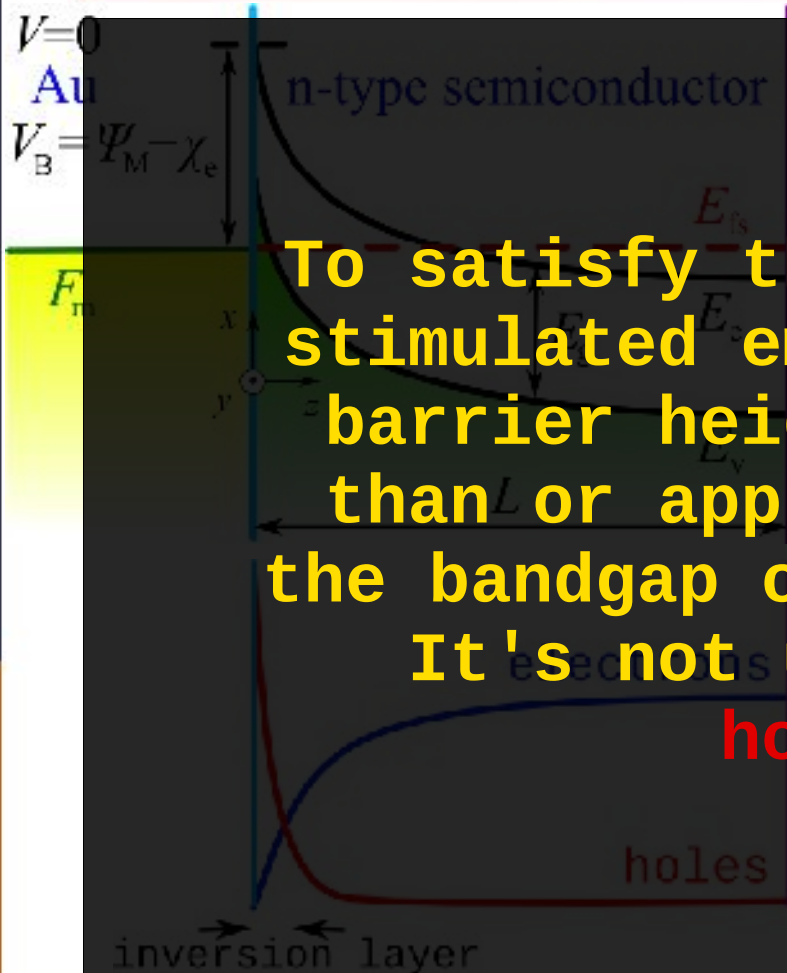
Condition for net stimulated emission or gain

$$F_e - F_h \geq \hbar \omega \geq E_g$$

-K.W. Nill et al., Appl. Phys. Lett. **16**, 375 (1970).

-D.Yu. Fedyanin and A.V. Arsenin, AIP Conf. Proc. **1291**, 112 (2010).

# SPP Amplification: Electric Pumping



To satisfy the condition for net stimulated emission or gain, the barrier height must be greater than  $L$  or approximately equal to the bandgap of the semiconductor. It's not usually possible, however  $F_e - F_h \geq \hbar \omega \geq E_g$

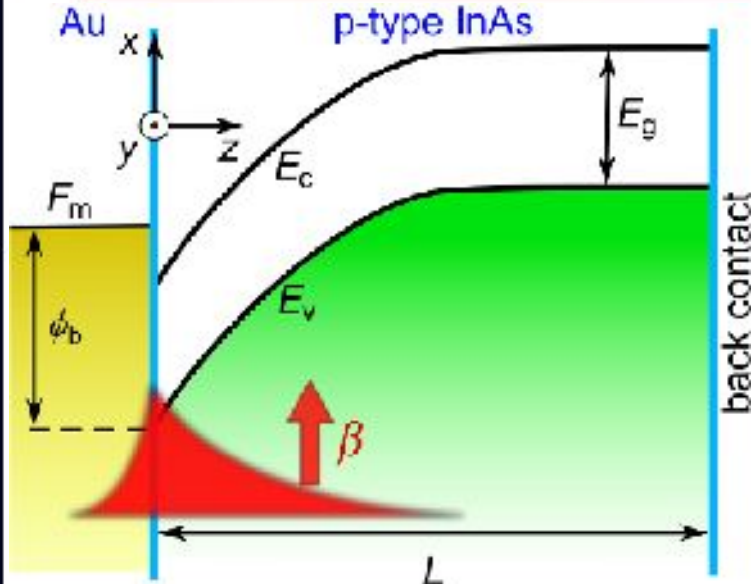
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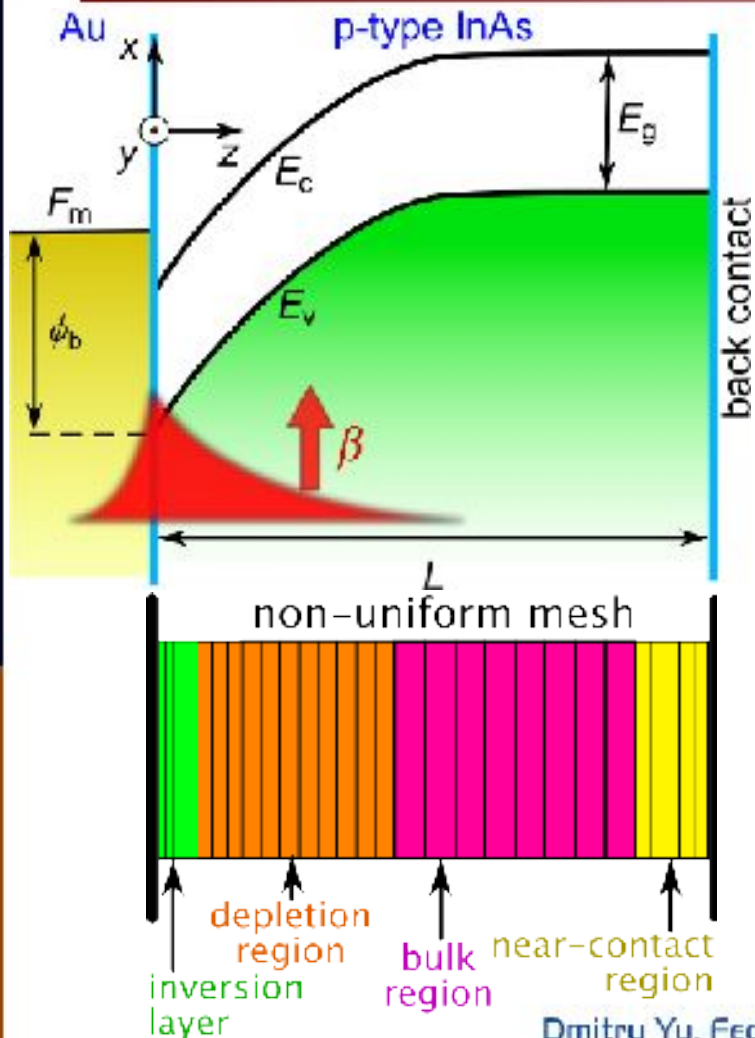
# SPP Amplification: Electric Pumping



Fermi level in the metal occurs 130 meV above the conduction band edge of InAs ( $E_g=0.40$  eV at 77K). Consequently, the barrier height of an Au/p-InAs contact is greater than the bandgap.

- D.Yu. Fedyanin, *Toward an electrically pumped spaser*, Opt. Lett. **37**, 404 (2012).
- D.Yu. Fedyanin, A.V. Arsenin, *Au/InAs Surface Plasmon Polariton Amplifier and SPASER* // AIP Conf. Proc. **1398**, 70 (2011)

# SPP Amplification: Electrical Pumping



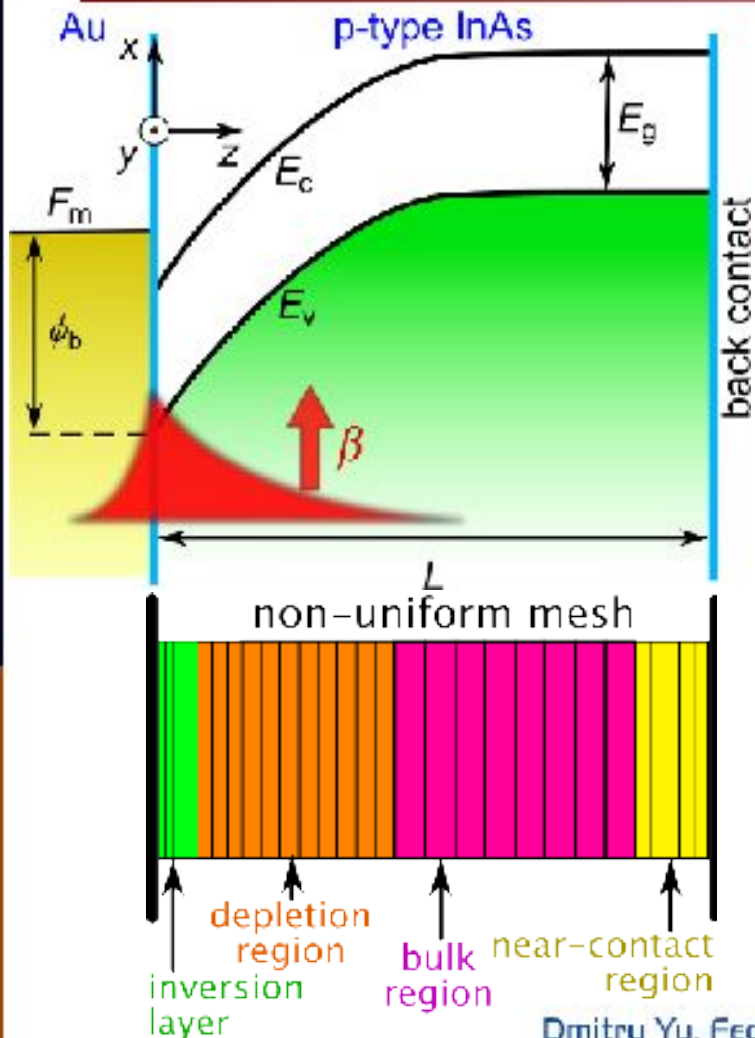
We solve six nonlinear first order differential equations that describe the carrier behavior within the semiconductor

$$\left\{ \begin{array}{l} d\phi/dz = -E_z \\ dE_z/dz = 4\pi e(p - n + N_d)/\epsilon_{st} \\ \frac{dn}{dz} = \frac{1}{eD_n} J_n - \frac{\mu_n n}{D_n} E_z \\ \frac{dp}{dz} = -\frac{1}{eD_p} J_p + \frac{\mu_p p}{D_p} E_z \\ dJ_n/dz = eU \\ dJ_p/dz = -eU \end{array} \right.$$

where  $U = U_{stim} + U_{spont} + U_{Auger}$



# SPP Amplification: Electrical Pumping



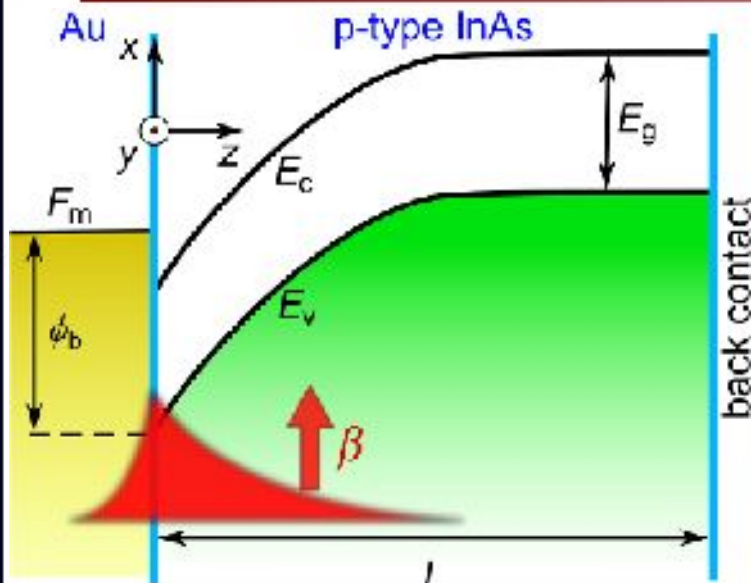
together with six boundary conditions

$$\left\{ \begin{array}{l} J_n |_{z=0} = e v_{nr} (n |_{z=0} - n_0) \\ J_p |_{z=0} = -e v_{pr} (p |_{z=0} - p_0) \\ \varphi |_{z=0} = -\frac{\psi_M - \chi_e}{e} \\ \varphi |_{z=L} = V + \frac{k_B T}{e} \ln \left( \frac{n_L}{N_c} \right) \\ n |_{z=L} = n_L \\ p |_{z=L} = p_L \end{array} \right.$$

where

$$v_{nr} \approx \frac{1}{4} \sqrt{\frac{8 k_B T}{\pi m_n}}; \quad v_{pr} \approx \frac{1}{4} \sqrt{\frac{8 k_B T}{\pi m_p}}$$

# SPP Amplification: Electrical Pumping



$$N_a = 2.33 \times 10^{18} \text{ cm}^{-3}$$

$$\hbar\omega = 0.3925 \text{ eV} (\lambda = 3.16 \text{ } \mu\text{m})$$

$$\tilde{n} = 3.50$$

$$L = 2.0 \text{ } \mu\text{m}$$

$$T = 77 \text{ K}$$

Stimulated emission and gain

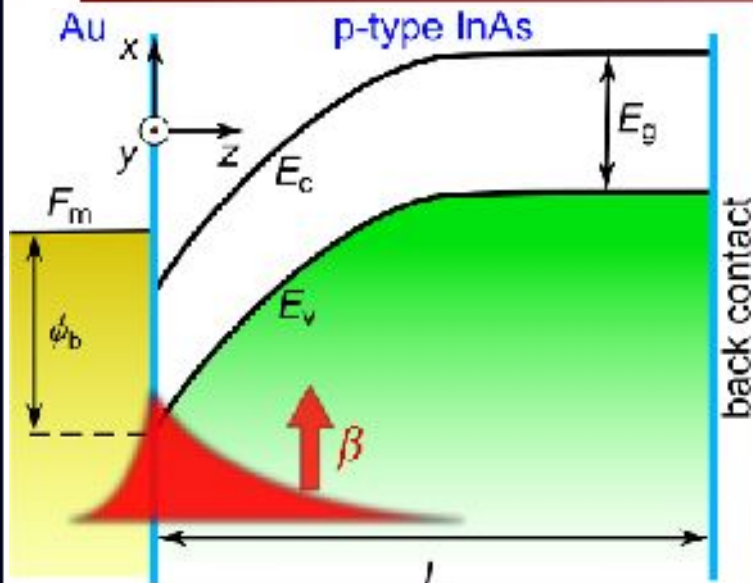
$$U = U_{\text{spont}} + U_{\text{Auger}} + U_{\text{stim}}$$

$$U_{\text{stim}}(z) = g(F_e(z), F_h(z)) S / \hbar\omega$$

$$g = \frac{4\pi^2 e^2}{c \tilde{n} m_{e0}^2 \omega} |M_b|^2 \int_0^{+\infty} |M_{\text{env}}(E, E - \hbar\omega)|^2 \rho_c(E - E_c) \rho_v(E_v - E + \hbar\omega) \times \left\{ \frac{1}{1 + \exp[(E - F_e)/k_B T]} - \frac{1}{1 + \exp[(E - \hbar\omega - F_h)/k_B T]} \right\} dE$$

- Gaussian Halperin-Lax band-tail (GHLBT) model
- Stern's envelope matrix element  $M_{\text{env}}$

# SPP Amplification: Electric Pumping



$$N_a = 2.33 \times 10^{18} \text{ cm}^{-3}$$

$$\hbar\omega = 392.5 \text{ meV} (\lambda = 3.16 \text{ }\mu\text{m})$$

$$\tilde{n} = 3.50$$

$$L = 2.0 \text{ }\mu\text{m}$$

$$T = 77 \text{ K}$$

Stimulated emission and gain

$$U = U_{\text{spont}} + U_{\text{Auger}} + U_{\text{stim}}$$

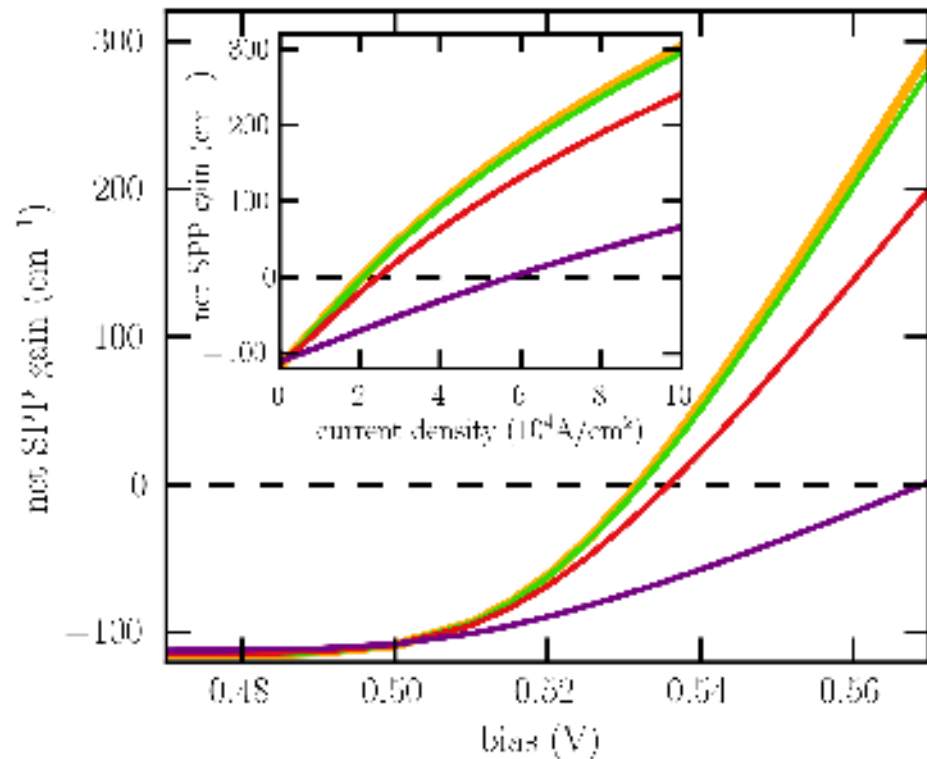
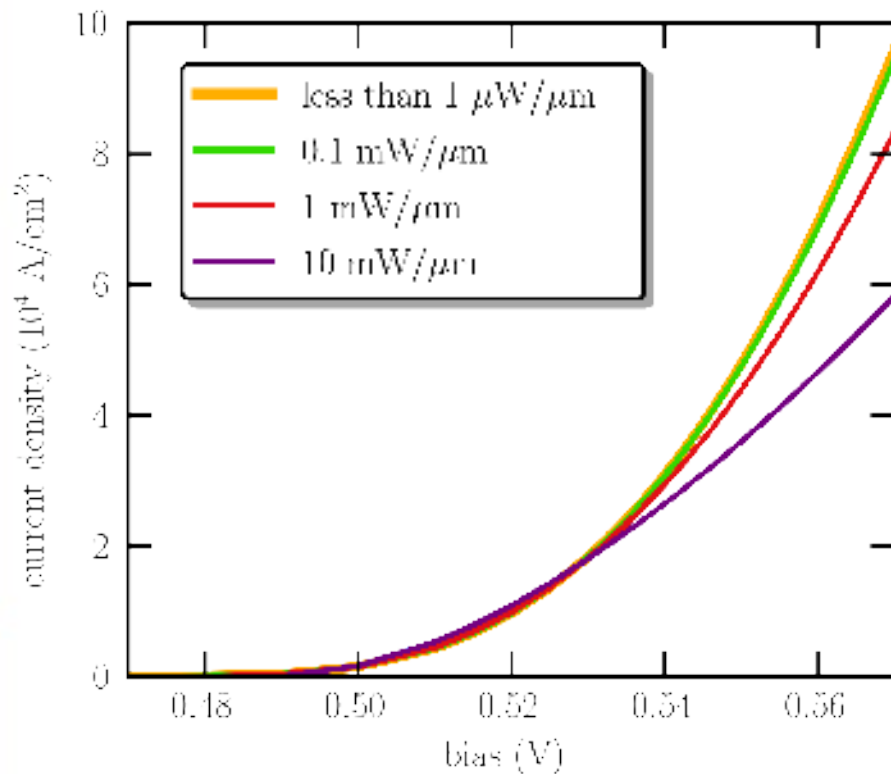
$$U_{\text{stim}}(z) = g(F_e(z), F_h(z)) S(z) / \hbar\omega$$

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$$\approx 1.41 \times 10^{-14} [\min(n, p) - 5 \times 10^{14}]$$

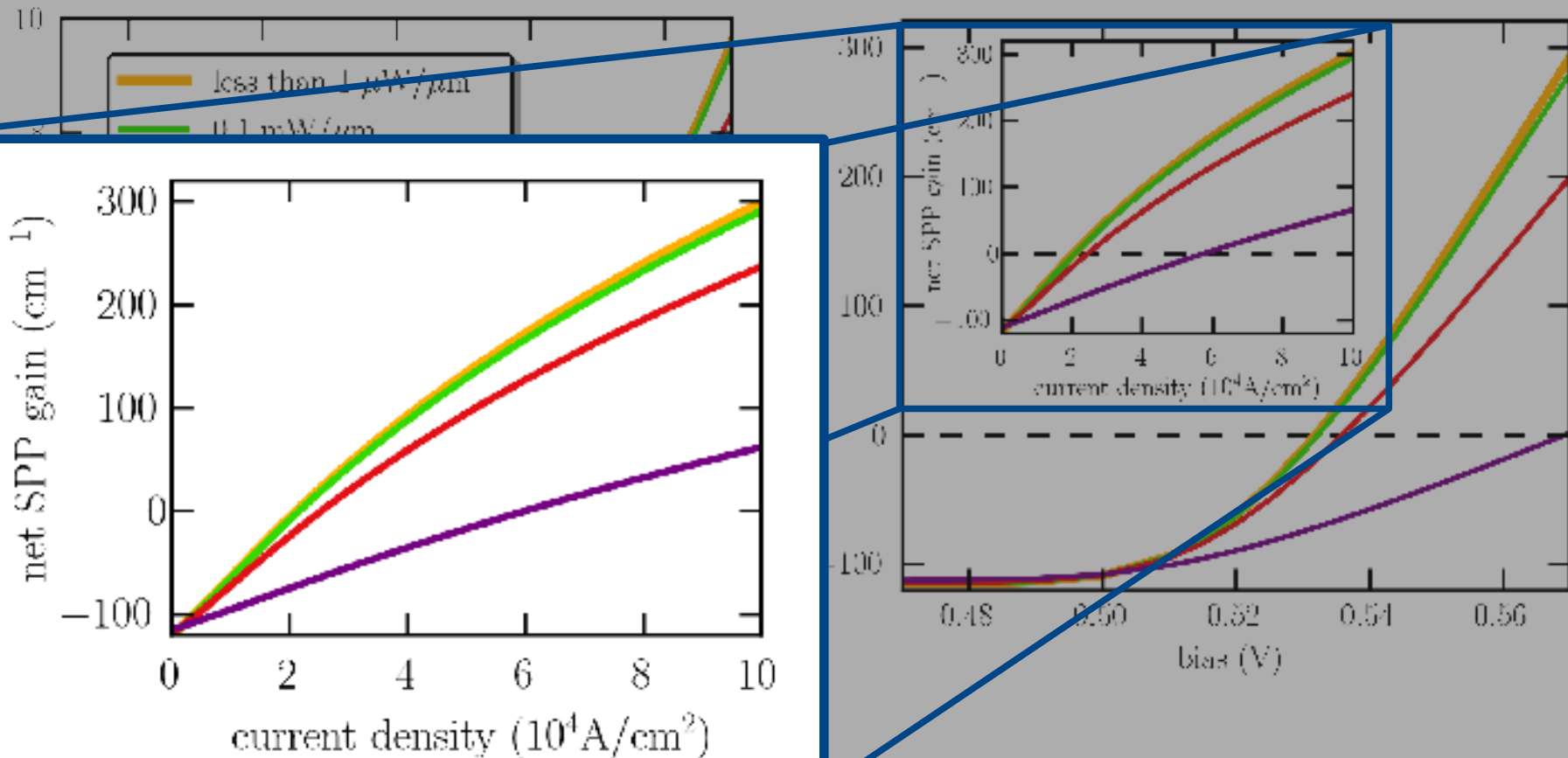
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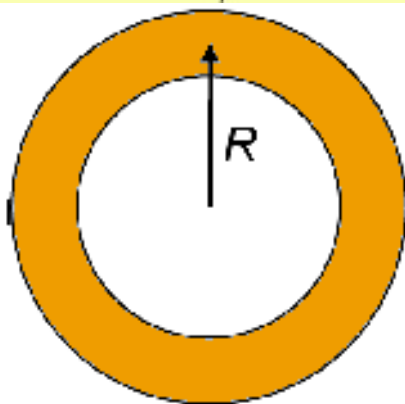
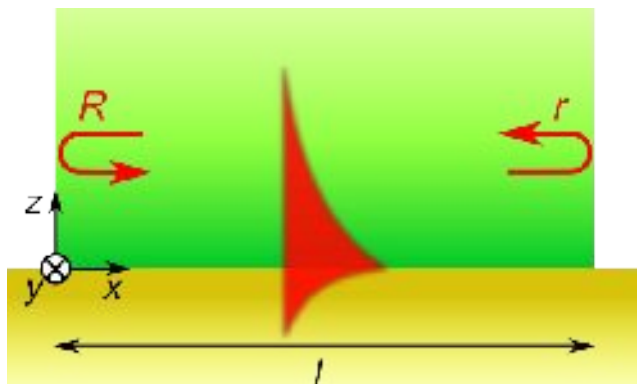


-D.Yu. Fedyanin, *Toward an electrically pumped spaser*, Opt. Lett. **37**, 404 (2012).

# Coherent SPP Sources

## *SP*PASER

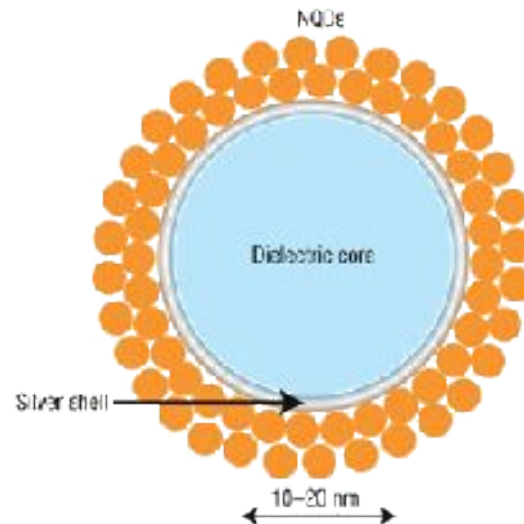
Propagating plasmons



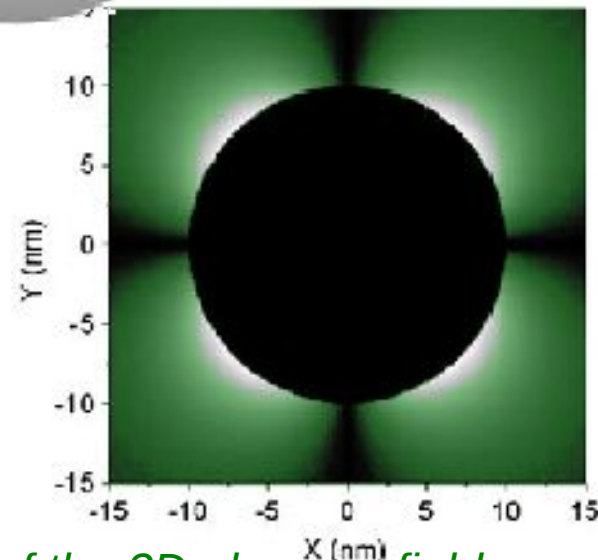
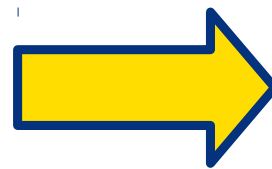
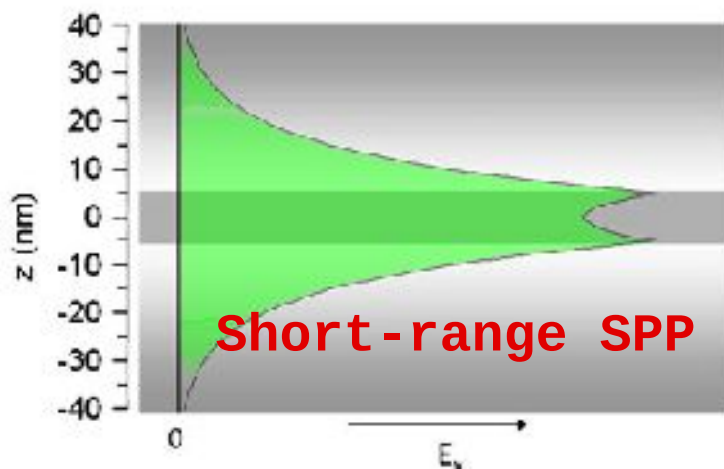
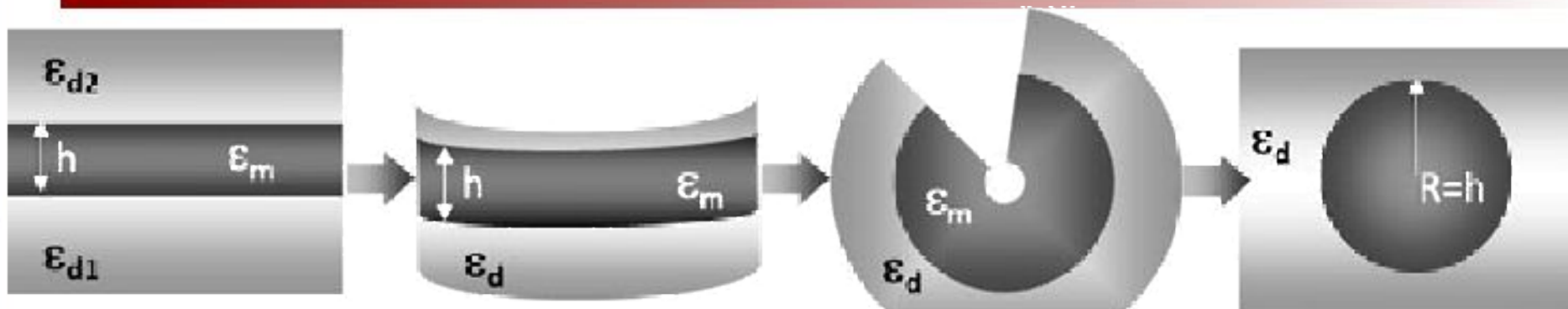
and

## *SP*PASER

Localized plasmons

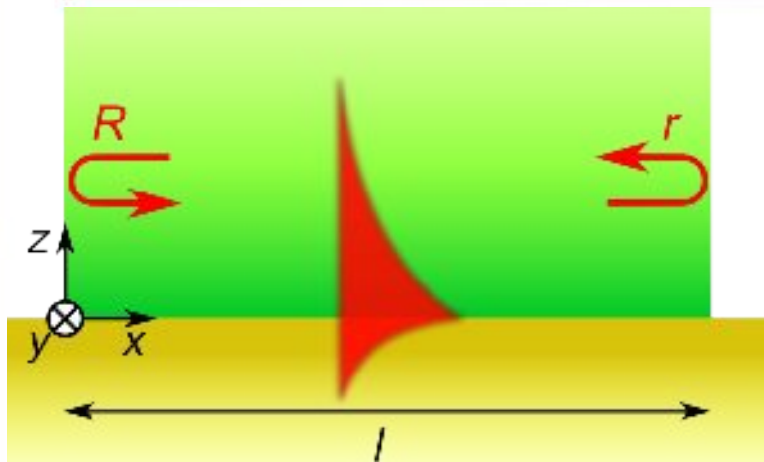


# SP<sub>P</sub>ASER and SPASER



-S. Bingham, R. Saudi, A.V. Tishchenko, *Extraction of the 3D plasmon field*, Plasmonics **6**, 445 (2011)

# SPASER



Threshold condition in a steady state:

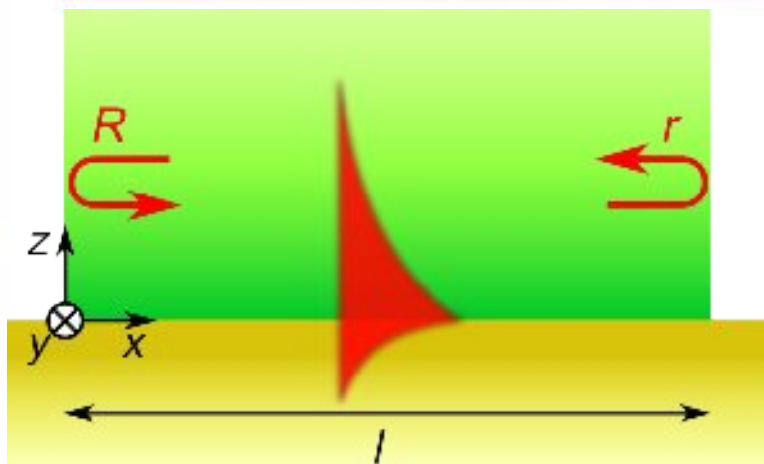
$$G_{\text{th}} = \frac{1}{2l} \ln \left( \frac{1}{|r|^2 |R|^2} \right)$$

Smooth facets:

$$|r|^2 = |R|^2 \approx \left| \frac{\frac{\beta c}{\omega} - 1}{\frac{\beta c}{\omega} + 1} \right|^2 = 0.31 \Rightarrow G_{\text{th}} = 115 \text{ cm}^{-1}, J_{\text{th}} = 4.4 \times 10^4 \text{ A/cm}^2 \text{ at } l = 100 \mu\text{m}$$



# SPASER

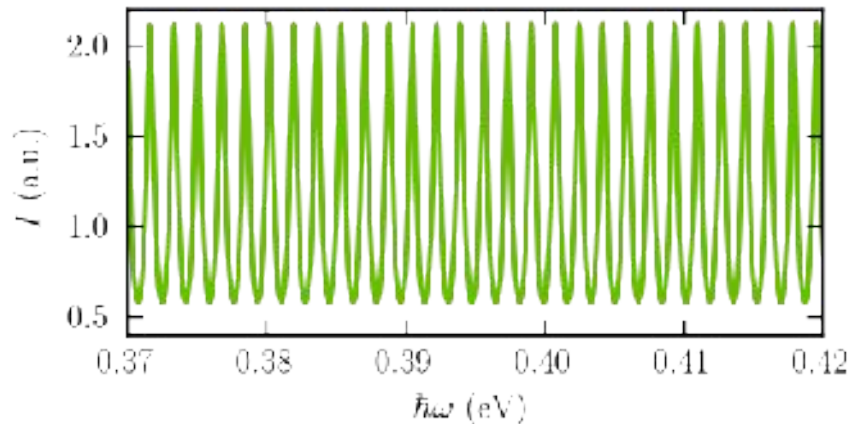
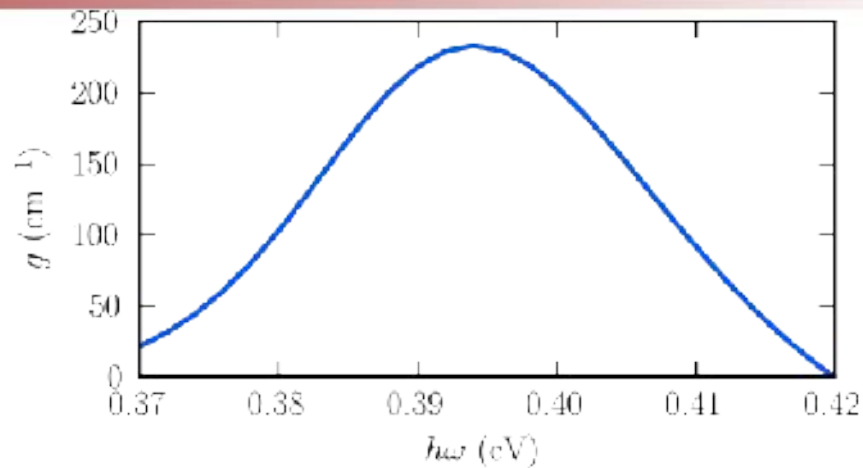


Threshold condition in a steady state:

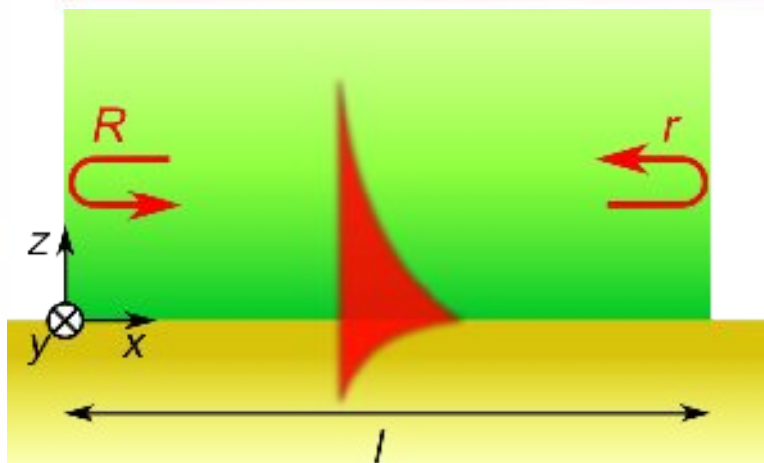
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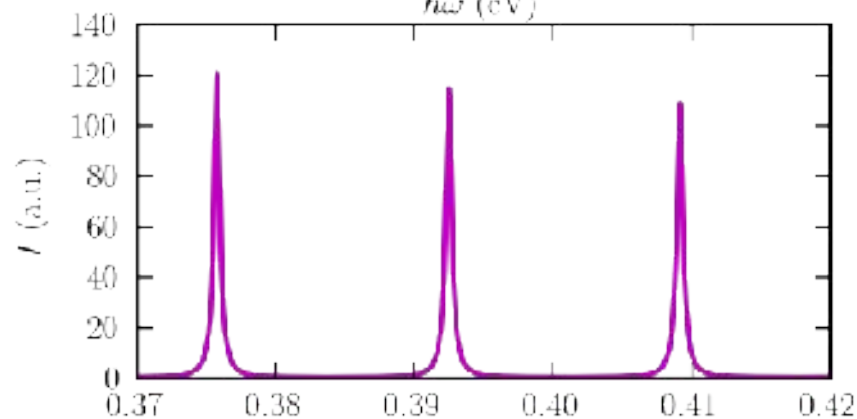
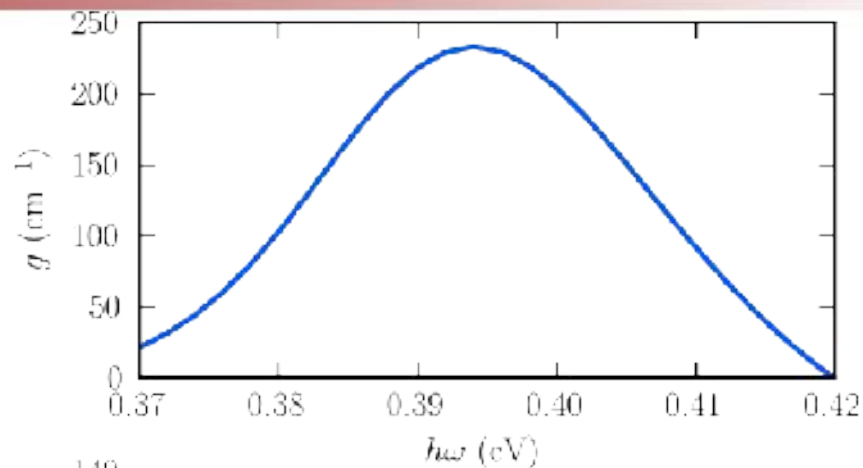


Threshold condition in a steady state:

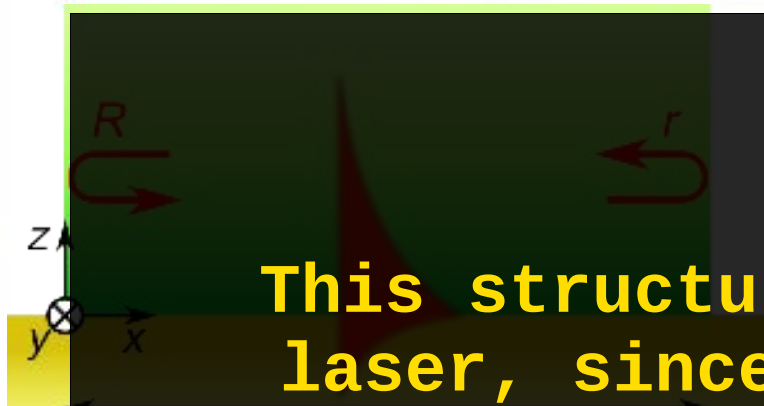
$$G_{\text{th}} = \frac{1}{2l} \ln \left( \frac{1}{|r|^2 |R|^2} \right)$$

15-nm Au coating:

$$|r|^2 = |R|^2 \approx \left| \frac{\frac{\beta c}{\omega} - 1}{\frac{\beta c}{\omega} + 1} \right|^2 = 0.9 \Rightarrow G_{\text{th}} = 95 \text{ cm}^{-1}, J_{\text{th}} = 4.0 \times 10^4 \text{ A/cm}^2 \text{ at } l = 10.2 \mu\text{m}$$



# SPASER



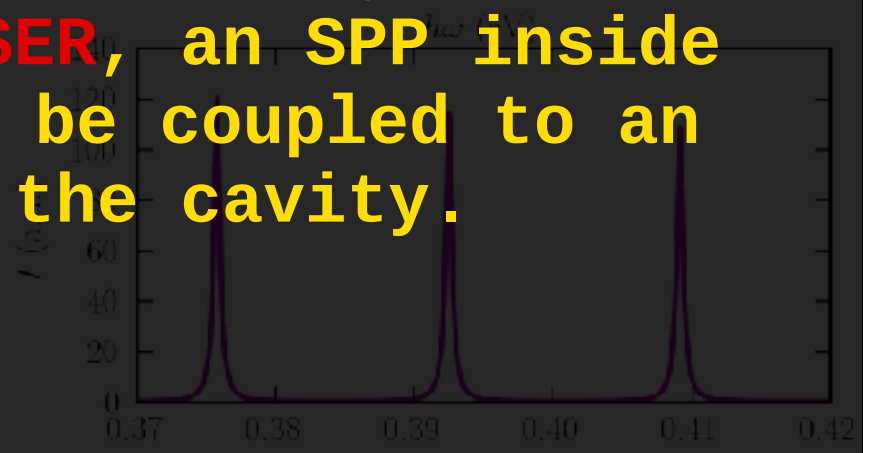
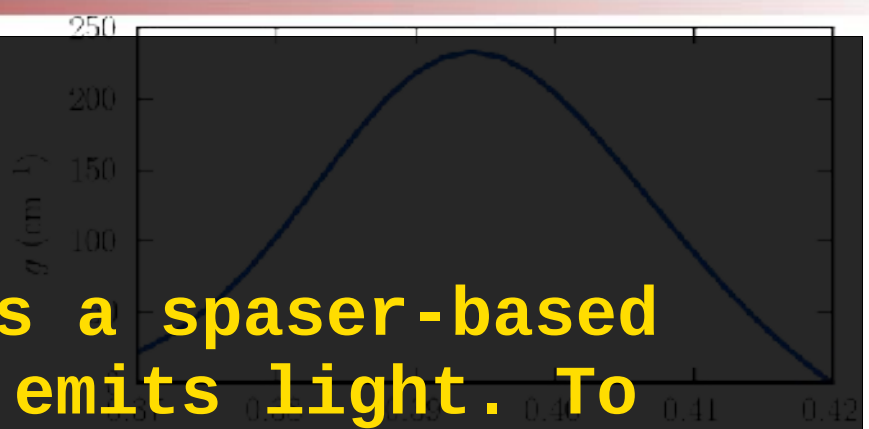
This structure is a spaser-based laser, since it emits light. To design a true SPASER, an SPP inside the cavity should be coupled to an SPP outside the cavity.

Threshold condition in a steady state:

$$G_{th} = \frac{1}{2l} \ln \left( \frac{1}{|r|^2 |R|^2} \right)$$

15-nm-thick Au mirrors:

$$|r|^2 = |R|^2 \approx \left| \frac{\frac{\beta c}{\omega} - 1}{\frac{\beta c}{\omega} + 1} \right|^2 = 0.9 \Rightarrow G_{th} = 95 \text{ cm}^{-1}, J_{th} = 4.0 \times 10^4 \text{ A/cm}^2 \text{ at } l = 10.2 \mu\text{m}$$



# SPASER

$$l = 10.2 \mu\text{m}$$

$$d = 20 \text{ nm}$$

$$D = 100 \text{ nm}$$

$$L = 2 \mu\text{m}$$

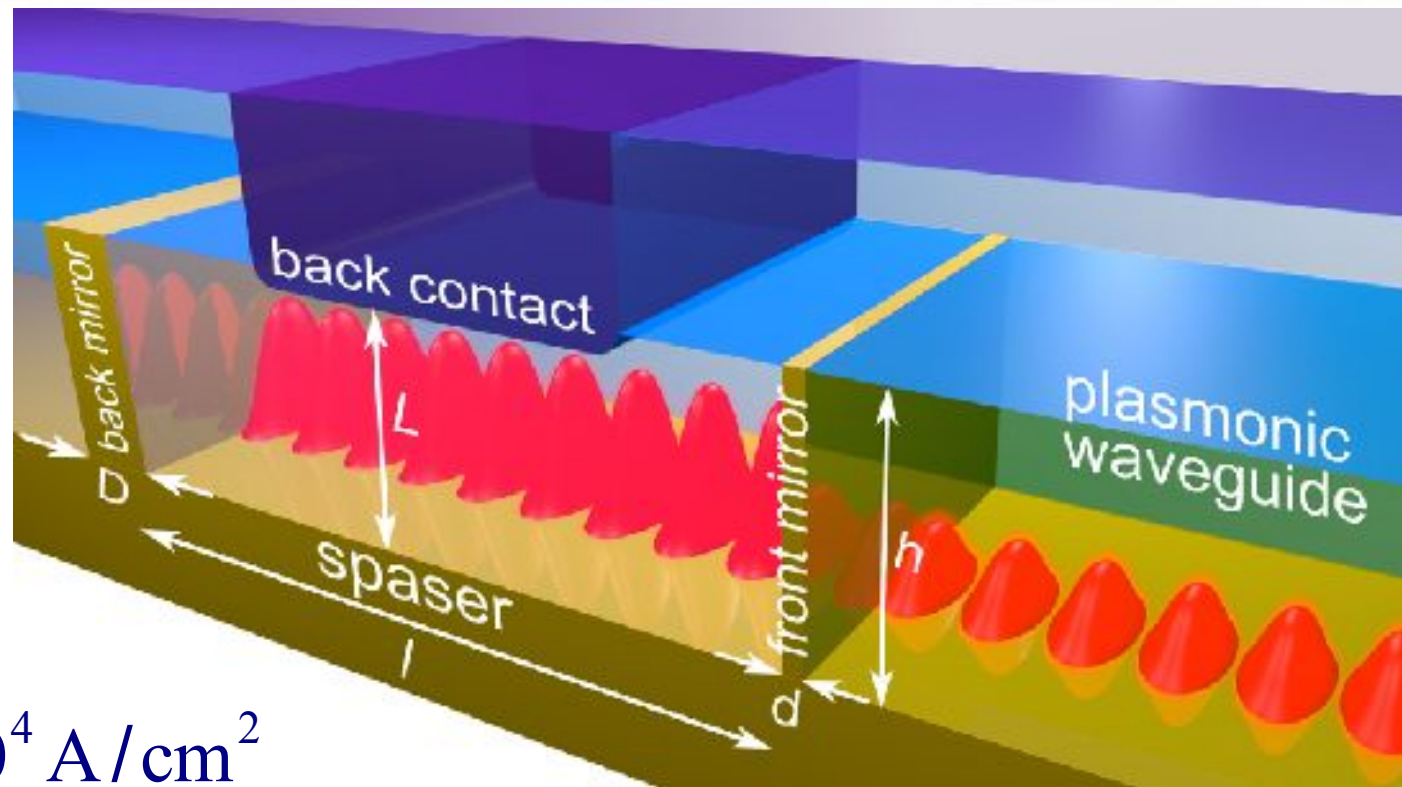
$$h \sim 2 \mu\text{m}$$

$$|R|^2 = 0.98$$

$$|r|^2 = 0.89$$

$$|t|^2 = 0.07$$

$$J_{\text{th}} = 3.3 \times 10^4 \text{ A/cm}^2$$



-D.Yu. Fedyanin, *Toward an electrically pumped spaser*, Opt. Lett. 37, 404 (2012).

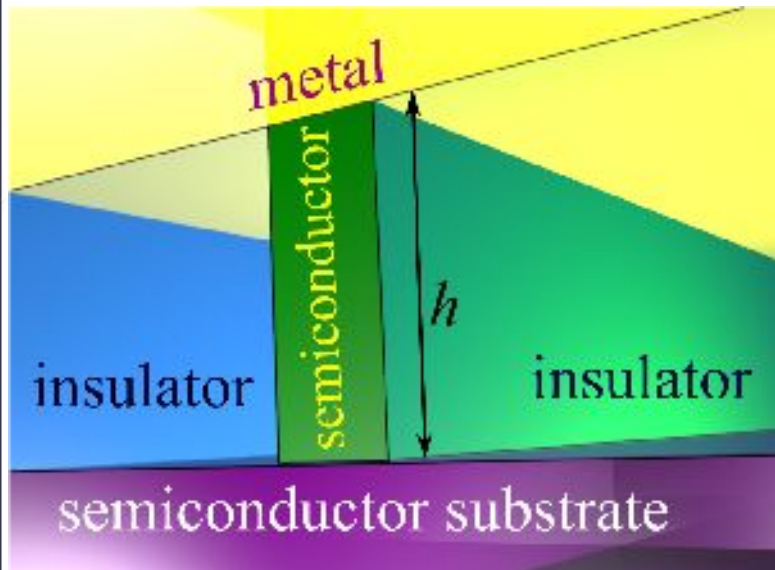
# Active Plasmonic Interconnects

What about of shrinking the lateral (y) dimension?



# Active Plasmonic Interconnects

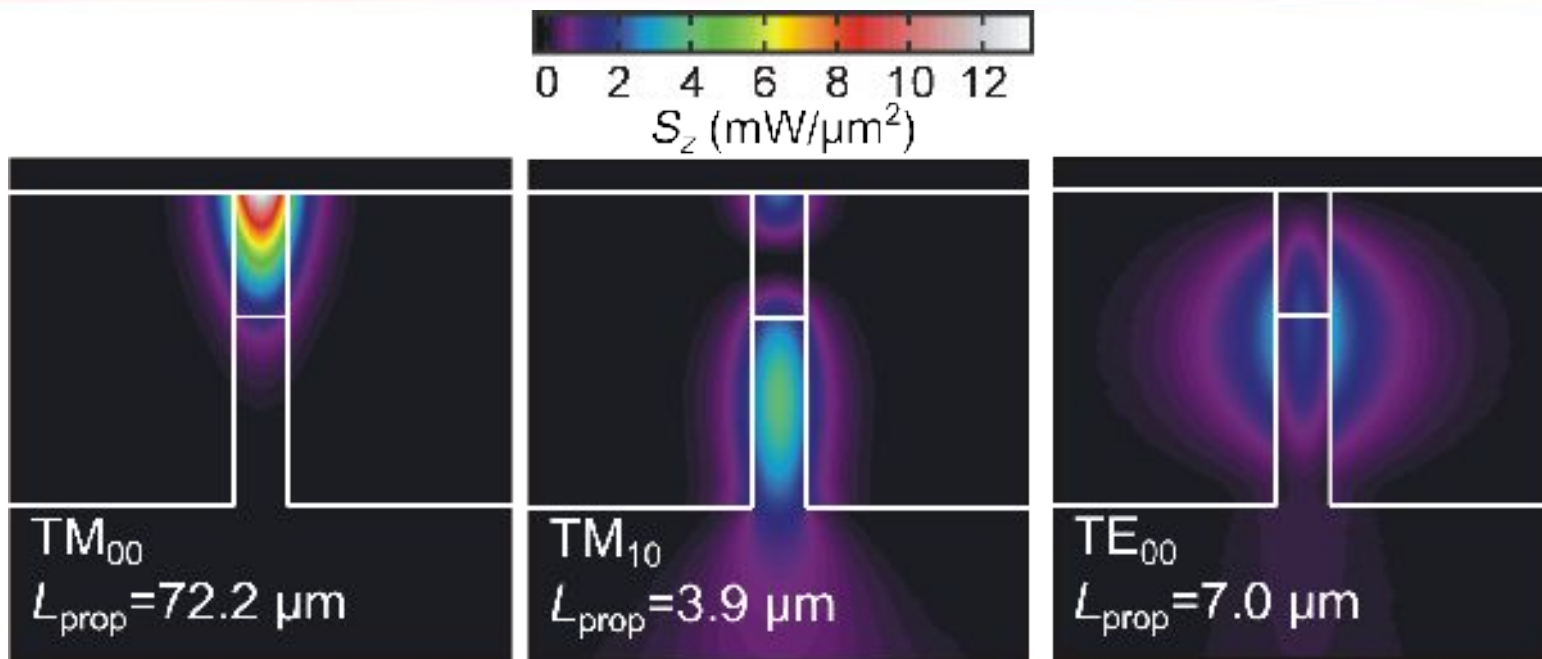
What about of shrinking the lateral (y) dimension?



All integrated circuits (both optical and electrical) are actually planar, 2D dimensional circuits. It means that *the mode height is not as important as the mode width*, which actually determines the crosstalk and integration density. So, we should decrease the waveguide width. In the present approach, there are no fundamental and technological

limitations for shrinking the lateral (y) dimension of the considered a structure down to several hundred nanometers, since there are only 2 characteristic dimensions: thickness of the inversion layer and thickness of the depletion region. Both of them are appreciably less than 100 nm.

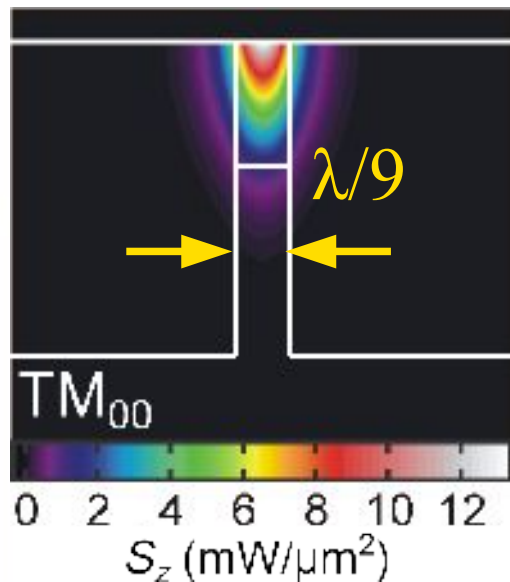
# Active Plasmonic Interconnects



Photonic  $\text{TE}_{00}$  and  $\text{TM}_{10}$  modes are very leaky modes and their propagation lengths are much shorter than propagation length of the plasmonic  $\text{TM}_{00}$  mode.

-D.Yu. Fedyanin, A.V. Krasavin, A.V. Arsenin, A.V. Zayats, *Surface plasmon polariton amplification upon electrical injection in highly integrated plasmonic circuits*, Nano Lett. (2012).

# Active Plasmonic Interconnects

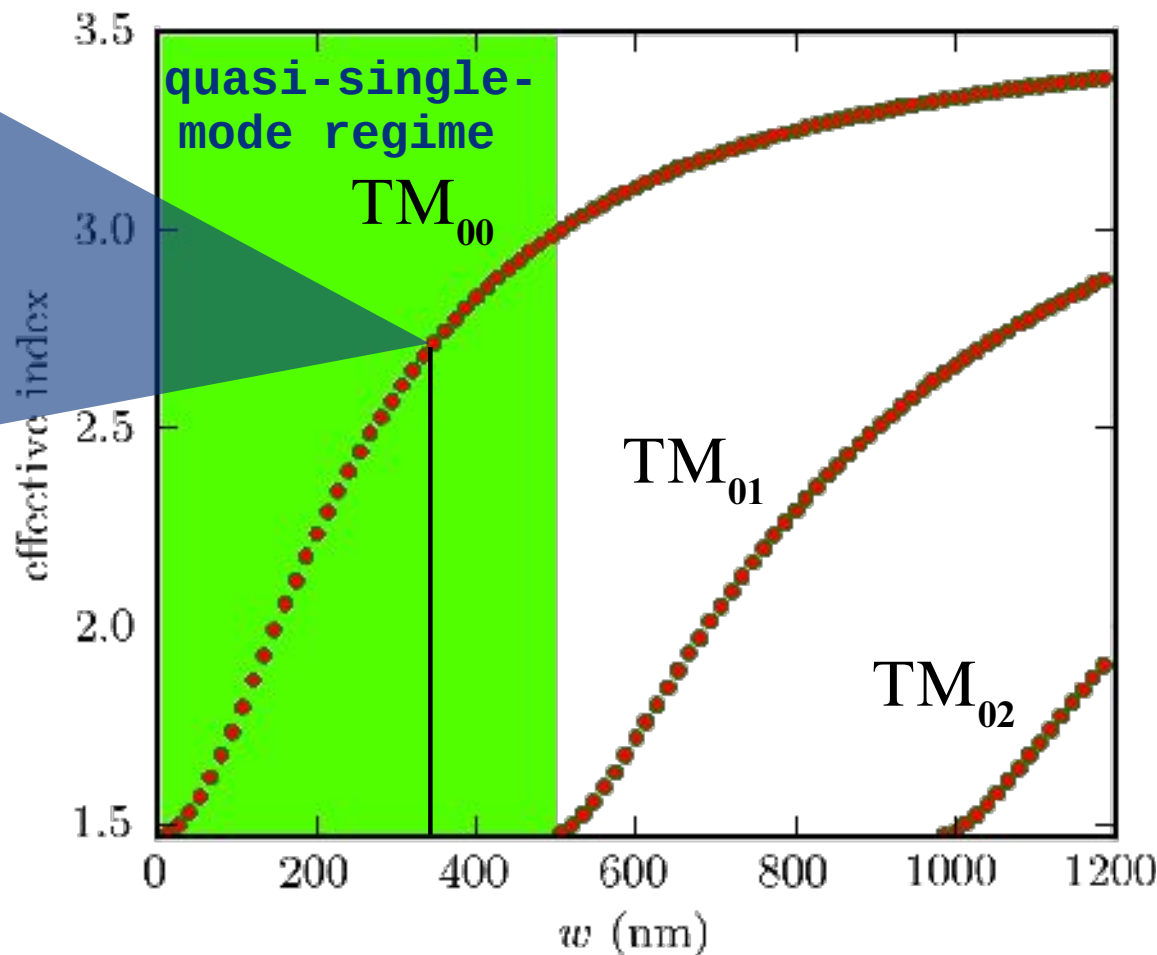


$$\epsilon_m = -535 + 35i \quad (\text{Au})$$

$$\epsilon_d = 2.16 \quad (\text{SiO}_2)$$

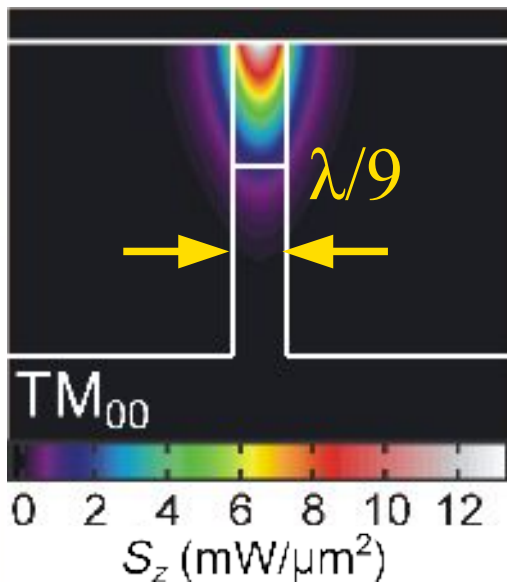
$$\epsilon_s = 12.25 \quad (\text{InAs})$$

$$\lambda = 3.16 \mu\text{m}$$





# Purcell Factor



$\tilde{n}(x, y)$  is real part of the refractive index of the medium at  $(x, y)$

$v_g$  is the SPP group velocity

$\xi(x, y)$  is approximately equal to  $\tilde{n}^2(x, y)$  in the semiconductor and in the insulator and equals  $1 + \omega_p^2 / (\omega^2 + \Gamma^2)$  in the metal.

$$F_p(x, y) = 1 + \frac{c^3 |E(x, y)|^2}{4\bar{n}(x, y)\omega^2 v_g \int_{-\infty-\infty}^{+\infty+\infty} \int_{-\infty-\infty}^{+\infty+\infty} \frac{1}{16\pi} \left( \xi(\tilde{x}, \tilde{y}) |E(\tilde{x}, \tilde{y})|^2 + |H(\tilde{x}, \tilde{y})|^2 \right) d\tilde{x} d\tilde{y}},$$

$$F_p(x, y) < 3.5$$

# Summary

- Despite the advantages of silicon photonics, even smaller interconnects are achievable with SPP based waveguides, which have the similar bandwidth and delays.
- SPP waveguides are quite lossy. However, one can partially or fully compensate losses using an active medium placed near the metal surface.
- Optical pumping is very bulky and cannot be used in nanoscale on-chip circuits and we should move to electric pumping.
- I've demonstrated an amplification scheme, which is based on a Schottky barrier diode that give a possibility to obtain net SPP gain.
- The presented approach give a possibility do design an electrically pumped SPASER.
- The obtained threshold current is relatively small for a pulsed and even a cw SPASER.
- There are no physical limitations for shrinking the lateral dimension of the proposed structure down to deep-subwavelength scale and development of on-chip plasmonic interconnects.



**Thank you for your attention!**

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